

TWO-STAGE PUMP WITH HIGH HEAD AND LOW DELIVERY

DESCRIPTION

The present invention relates to a two-stage pump  
5 with a high head and low delivery.

In the sector in question particular types of pump  
(called PEP, i.e. Partial Emission Pumps) are known,  
said pumps having the characteristics of a high head  
and low delivery and being of the type where a fluid,  
10 contained in a tank and subject to the pressure  
determined by the fluid column, enters into the pump in  
an axial direction and is pushed by the impeller  
towards the delivery duct arranged in a tangential  
direction and having dimensions such as to determine  
15 the required head of the pump.

It is also known that, in order to be able to  
increase the head of the pump, it is possible to modify  
only the number of revolutions of the impeller which,  
consequently, must be designed with a special form able  
20 to ensure that the inlet pressure is maintained;  
otherwise, the increase in the number of revolutions  
would result in a reduction in the inlet pressure and  
consequently a reduced intake of fluid with a  
consequent decrease in the efficiency of the pump; this  
25 effect is even more marked in those cases where the  
pump is arranged at a level higher than that of the  
free surface of the fluid to be drawn.

In order to overcome this drawback, high-speed  
pumps have been designed, of the type provided with a  
30 fast main impeller able to increase substantially the  
head and an auxiliary impeller arranged upstream of the  
first impeller and able to supply the main impeller  
without a substantial loss in suction of the fluid at  
the inlet and without affecting the increase in the  
35 delivery pressure of the pump.

These pumps, however, are complicated and costly

to manufacture and moreover require special parts with a limited degree of standardization.

The technical problem which is posed, therefore, is that of designing pumps which are able to operate  
5 within a wide range of low delivery values and with a high head, without being affected by the abovementioned problems of the existing art.

Within the context of this problem a further requirement is that the pump should have compact  
10 dimensions and have high interchangeability characteristics, namely should allow variation in the rated delivery within a wide range of operating values, with minimum modifications which do not involve the general structure of the pump and allow the largest  
15 possible number of components to be standardized, reducing in this way the storage requirements and consequently the production and management costs.

These results are obtained according to the present invention by a pump comprising a body, an  
20 actuating shaft, on which at least a first impeller and a second impeller are coaxially mounted, each being housed in a respective front chamber and rear chamber respectively connected to a fluid intake duct and a fluid delivery duct, in which said front chamber is  
25 delimited by said body and by an interstage body, said rear chamber is delimited by said interstage body and by a shield, said interstage body has two volutes respectively associated with the corresponding first impeller and second impeller, a first discharge orifice  
30 connecting the volute of the first impeller to the exterior, a second discharge orifice connecting the volute of the second impeller to the delivery duct, inside said body there being formed a channel for the throughflow of the fluid from said first chamber to the  
35 means for supplying the fluid to the second impeller.

Further details may be obtained from the following

description of a non-limiting example of embodiment of the subject of the present invention provided with reference to the accompanying drawings, in which:

5       - Figure 1 shows a partially sectioned schematic perspective view of the pump according to the present invention;

      - Figure 2 shows a partially sectioned schematic perspective view of the pump according to Fig. 1;

10       - Figure 3 shows a schematic cross-section through the pump according to Fig. 1.

      As shown in Fig. 1, the pump according to the present invention comprises a body 10 with which the duct 11 for axial entry of the fluid is associated;  
15       said duct 11 is formed inside a coaxial extension 12 provided with a flange 12a for frontal coupling with the supply apparatus.

      For the sake of convenience of description said part corresponding to the body 10 of the pump and to  
20       the fluid inlet will be defined below as "front", while the opposite side will be defined as "rear".

      Said front body 10 also contains the fluid delivery duct 13 which extends in a direction tangential to the said body 10 inside a corresponding  
25       extension 14 with which an associated coupling flange 14a is integral.

      A suitable annular seat 15 is formed in the body 10 and has, arranged therein, a coaxial interstage body 16 through which the pump actuating shaft 1 passes via  
30       a bush 1a.

      Said interstage body 16 essentially divides the annular seat 15 into a first front chamber 15a and into a second rear chamber 15b; inside these chambers a first impeller 21a and a second impeller 21b  
35       respectively rotate, being both mounted on the said actuating shaft 1; said impellers are identical,

symmetrical and opposite to each other.

5 Said chambers 15a, 15b communicate with the exterior by means of respective volutes 22a and 22b which, in a preferred embodiment, are of the annular type, have a constant cross-section and have discharge nozzles 16a, 16b which are angularly offset at 180° with respect to each other.

10 Said second chamber 15b is closed at the rear and axially closed by a shield 23 inside which (Figs. 2 and 3) a radial duct 24 is formed; one external end 24b of said duct is connected to a channel 17 which is parallel to the longitudinal axis of the pump and formed in the front body 10 thereof and the other internal end 24a is connected to a coaxial annular header 25 which emerges coaxially in said rear chamber 15b.

20 The front chamber 15a is connected to the said axial duct 17 of the body 10 by means of a volute 22a, the said discharge nozzle 16a formed in the interstage body 16 and arranged in a tangential direction, and a radial duct 16c; the rear chamber 15b is in turn connected to the tangential delivery duct 13 by means of the volute 22b, the associated discharge nozzle 16c formed in a tangential direction in the interstage body 25 16 and a corresponding radial duct 16d formed in the body 10 of the pump.

30 The shield 23 also has a coaxially extending seat 23a in which it is possible to mount all the sealing devices on the shaft, whereby the possibility of installing magnetic-coupling drive devices necessary for highly dangerous, radioactive and similar fluids is also envisaged.

35 The pump is closed at the rear by a casing 30 acted on by a flange 31 which ensures clamping of the shield 23 and the interstage body 16 in the axial direction.

The supports 40 of the shaft 1 are fastened on the other side of the casing 30. Said parts of the pump are conventional per se and therefore not described in detail.

5 The operating principle of the pump is as follows:

- the fluid which enters via the intake duct 11 reaches the first chamber 15a where it is subjected to the action of the first impeller 21a which pushes it into the volute 22a and from here into the duct 16a,16b  
10 for connection to the channel 17 which emerges in the radial duct 24 of the shield 23;

- along this first travel path the fluid undergoes the first increase in pressure with respect to the intake pressure;

15 - upon leaving the radial duct 24 the fluid is forced inside the annular header 25 which arranges it in the axial direction for entry into the second chamber 15b where it is subjected to the action of the second impeller 21b which forces it into the volute 22b  
20 and from here into the radial duct 16c,16d and then into the delivery duct 13 with a further increased pressure.

It is pointed out therefore how the two impellers and the associated concentric volutes produce a series  
25 action on the fluid able to increase its head (typical values of up to 200m of liquid column) without an increase in the number of revolutions of the impellers and therefore without a reduction in the intake characteristics of the pump which may continue  
30 operating close to the point of maximum efficiency with advantages in terms of energy and fluid dynamics.

In addition to this, the pump according to the invention allows a high degree of interchangeability since it is possible to vary the rated delivery of the  
35 pump (typical values ranging from 1 to 18 m<sup>3</sup>/h) by simply changing the interstage body 16 and keeping

unchanged the configuration and the dimensions of the other parts of the pump, which also has a rotating part which, owing to the symmetry and opposite positioning of the impellers and the arrangement of the nozzles of the two volutes at 180°, is substantially free from the effect of radial and/or axial loads with a consequent increased structural rigidity which favours the working life of the sealing parts and the parts subject to wear, increasing the reliability of the pump.

The pump according to the invention has moreover an extremely compact design among other things owing to the formation, inside the body, of the duct connecting the two stages, avoiding the excessively large dimensions resulting from the external connection channels of the conventional type.

It is pointed out moreover how the pump body 10 has a configuration of the housing in the form of a radially divided "barrel" with flanged intake and delivery openings having the function of withstanding the rated pressure and housing the two impellers and the interstage body containing the two concentric volutes with respective diffusion channels and the rear shield inside which the radial interstage connection channel, the intake header and the chamber housing the shaft sealing device are formed.

In a preferred embodiment it is envisaged that the seal between the body 10 and the shield 23 and the seal between the zones subject to the differential pressures of the first and second stage consist of seals 50 of the spiralled metallic type, made on the one hand of steel and on the other hand of graphite and able also to take up any play resulting from the mating or thermal expansion and/or contraction of the various parts.